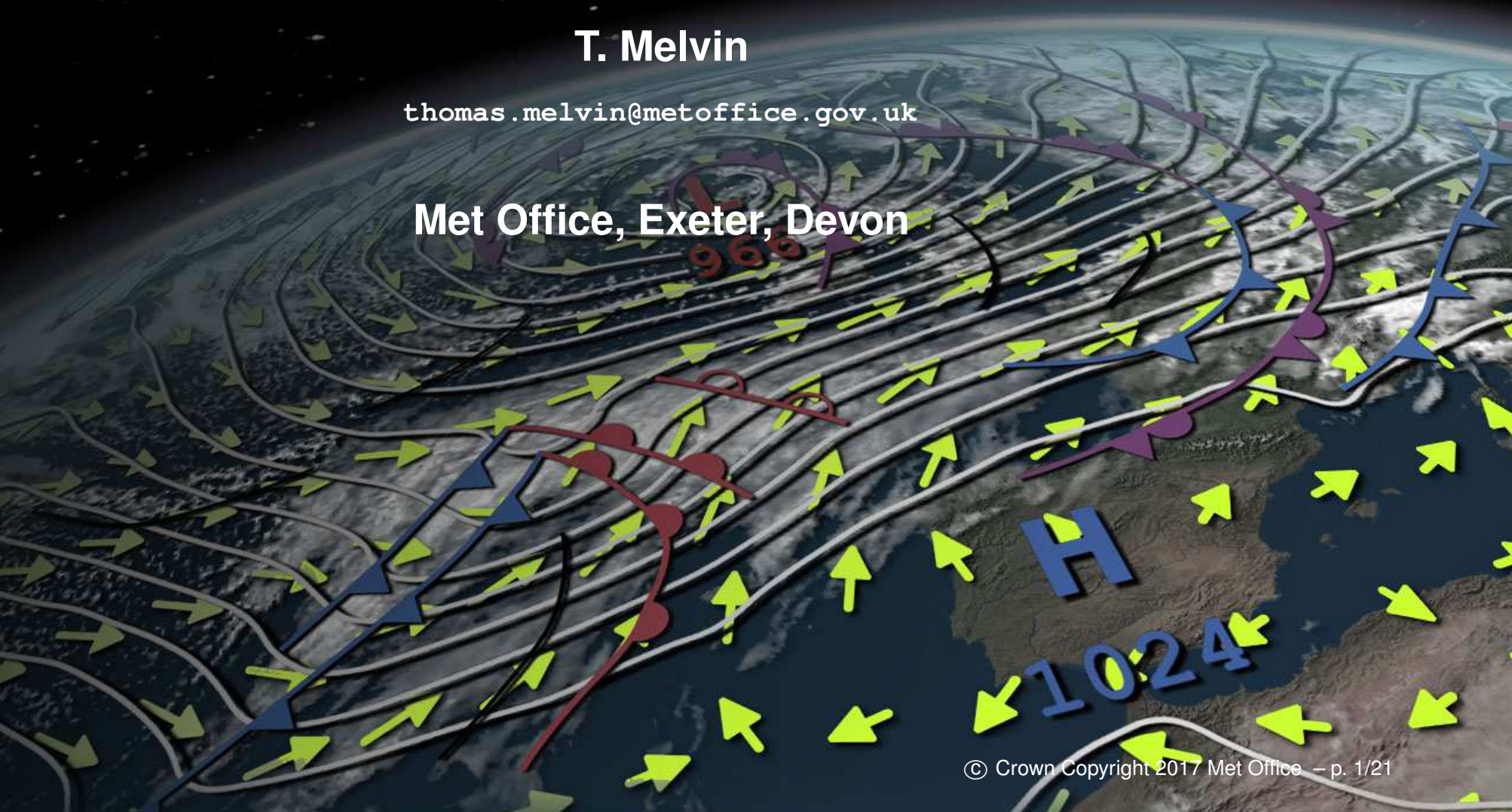


Atmospheric Modelling

T. Melvin

`thomas.melvin@metoffice.gov.uk`

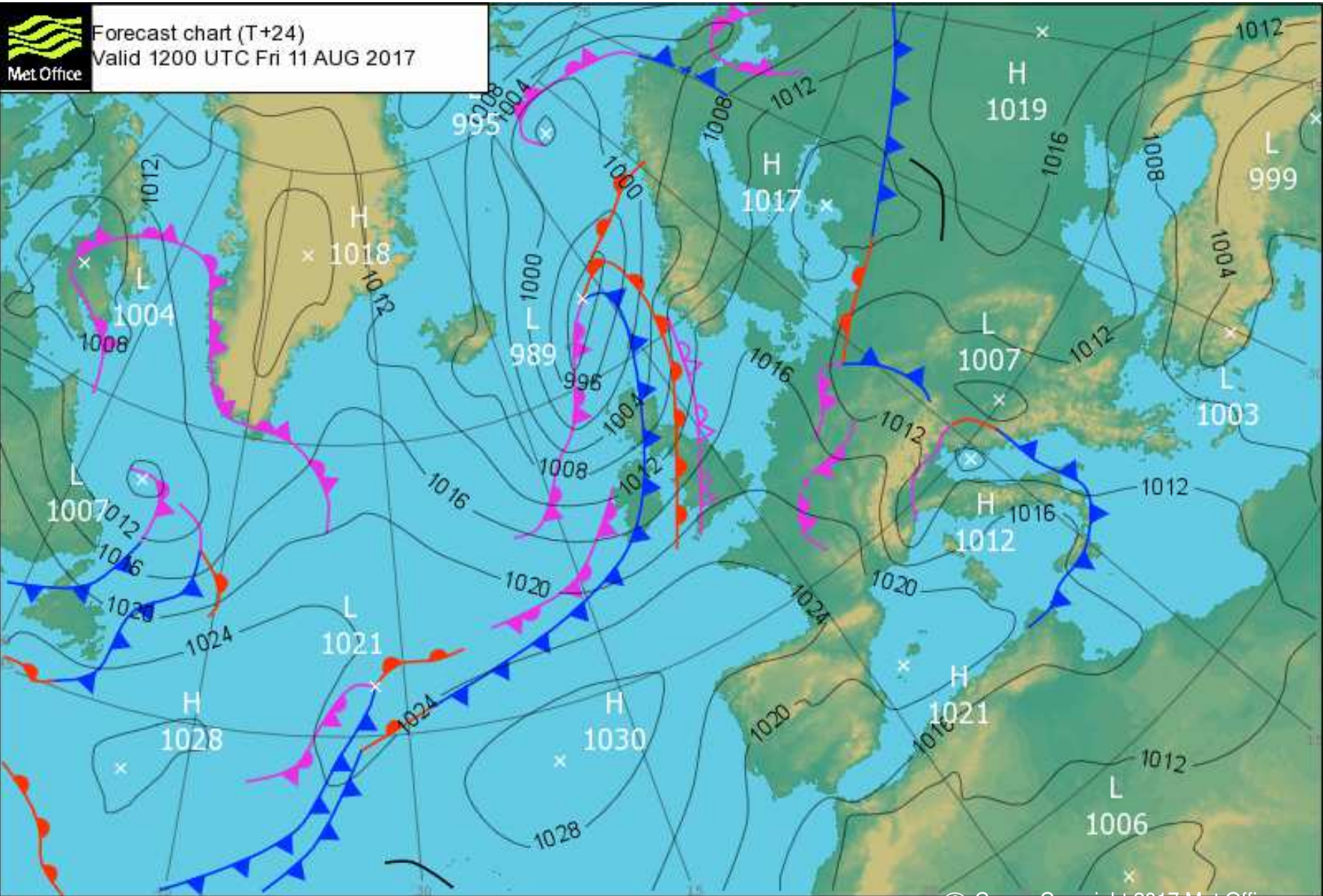
Met Office, Exeter, Devon



Today's Weather

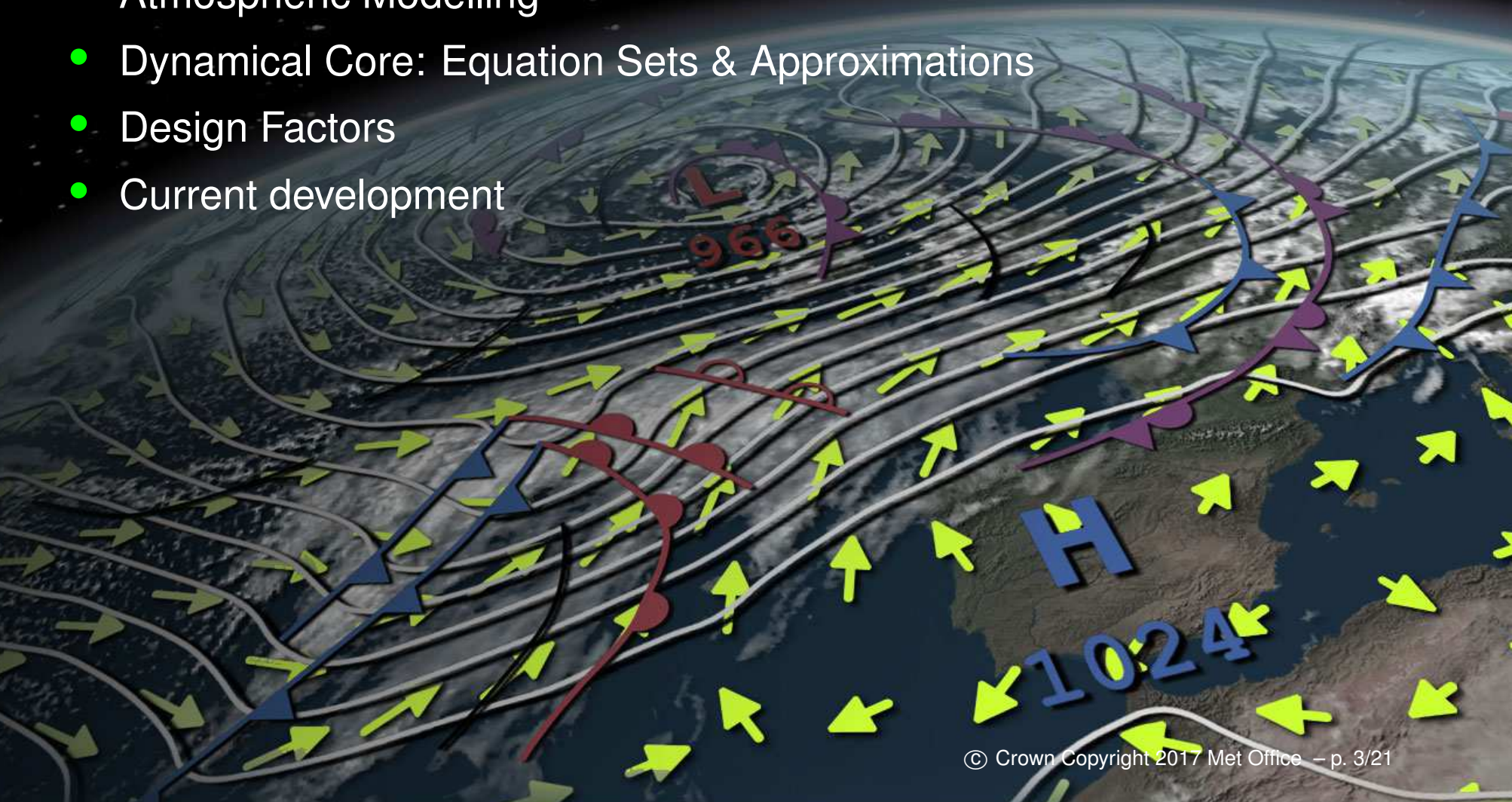


Forecast chart (T+24)
Valid 1200 UTC Fri 11 AUG 2017

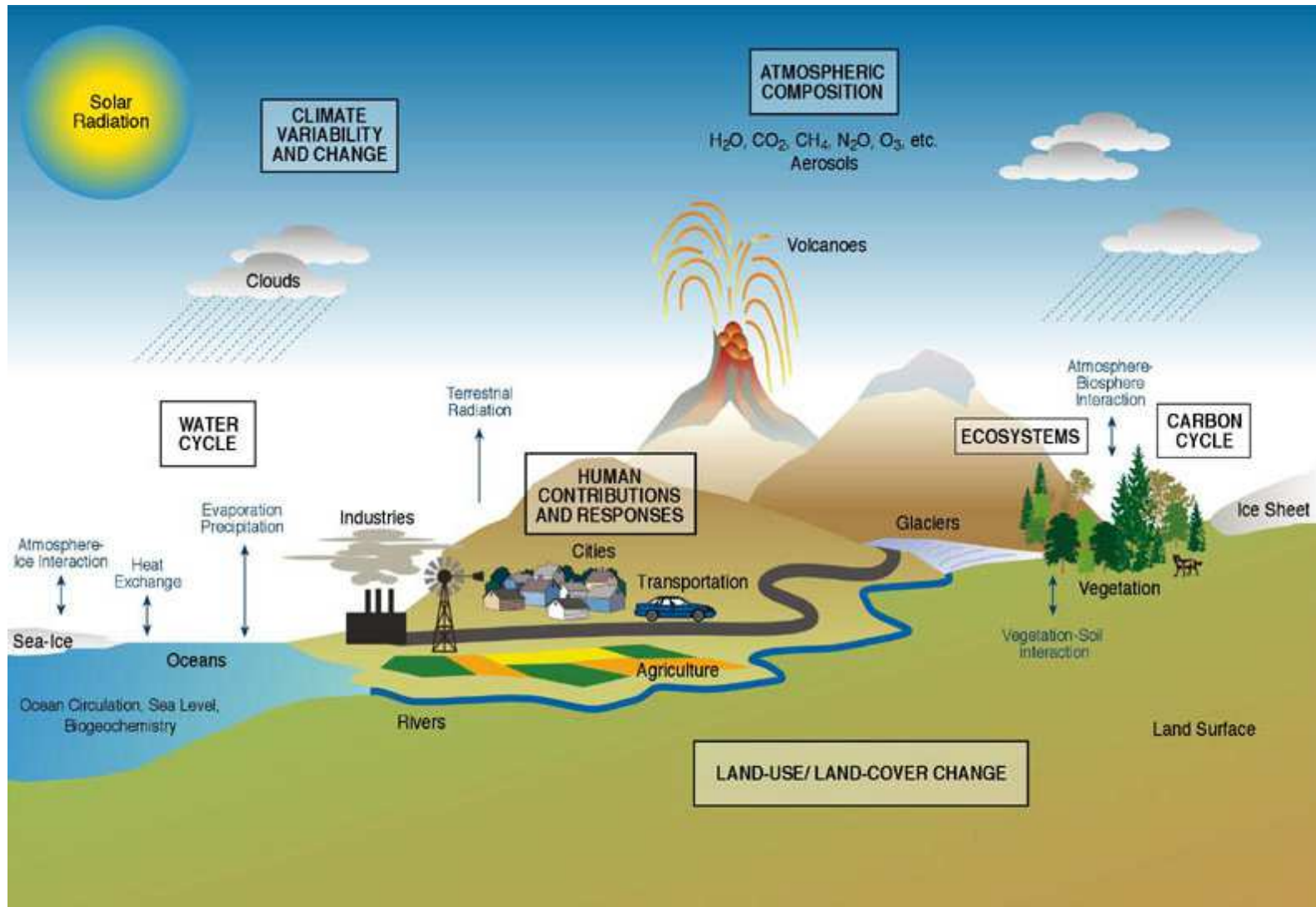


Overview

- Weather and Climate modelling: System Complexity
- Met Office approach to modelling
- Atmospheric Modelling
- Dynamical Core: Equation Sets & Approximations
- Design Factors
- Current development



System Complexity: Physical



System Complexity: Model

Data Assimilation
and Ensembles

Biogeochemistry

I/O

ENDGame
(Dynamical Core)

NEMO
Ocean

JULES
(Land Surface)

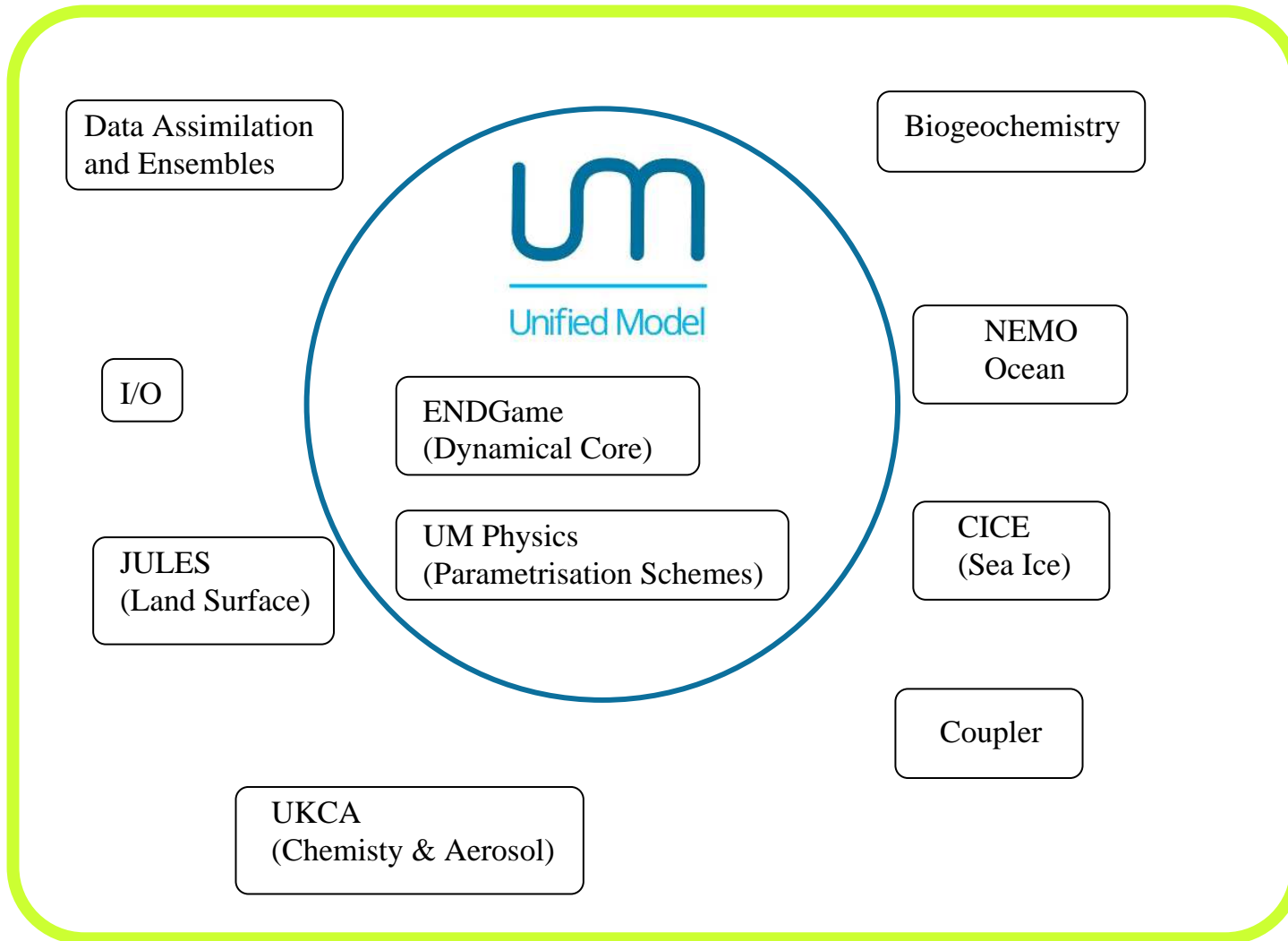
UM Physics
(Parametrisation Schemes)

CICE
(Sea Ice)

UKCA
(Chemistry & Aerosol)

Coupler

System Complexity: Model



Met Office Approach: Unified Model (UM)

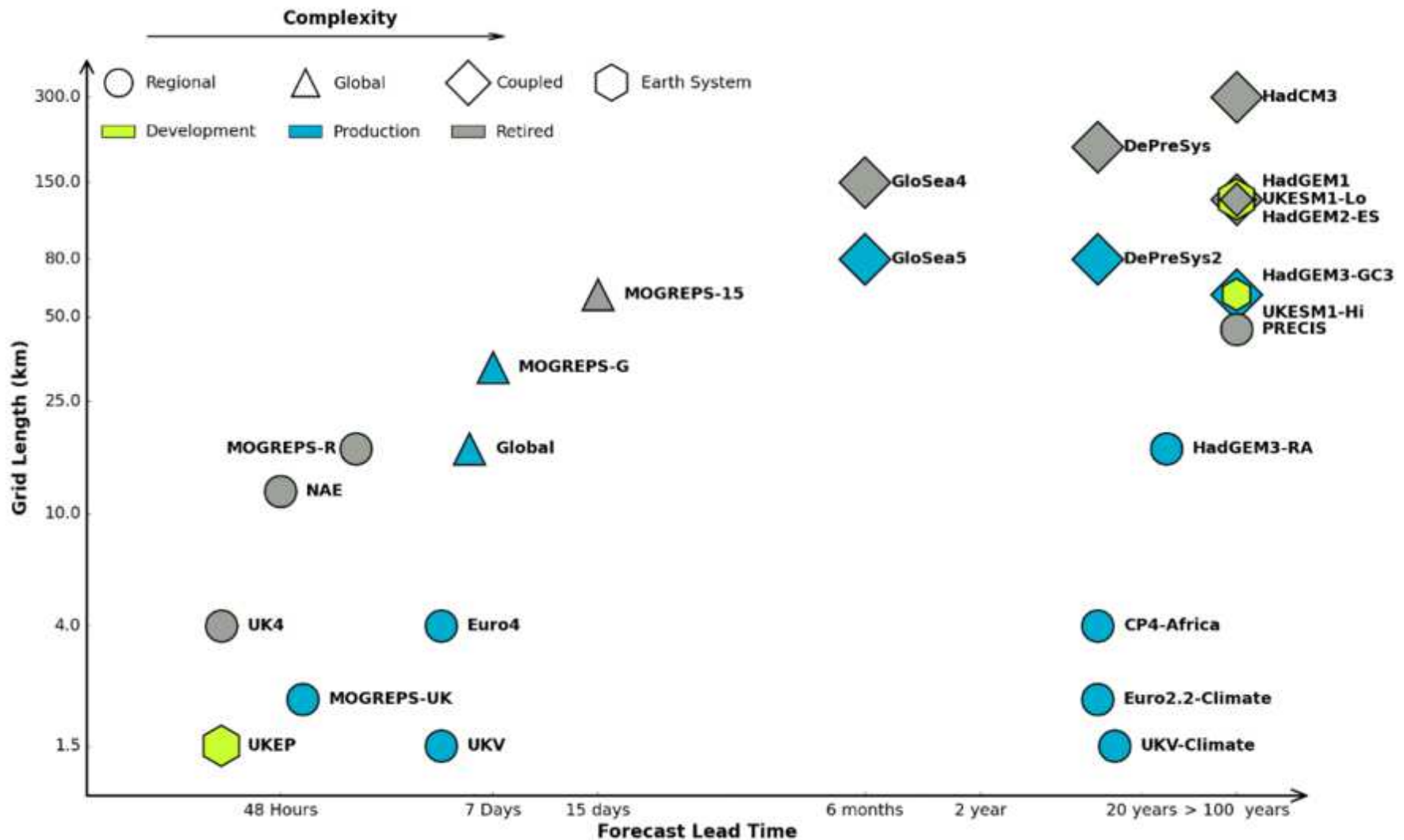
Single Model (Single numerics, Single source code) for all time and space scales

Climate Modelling: up to 100's Km for 1000's Years

Weather Forecasts: 1-10 Km for 5 days

Process Studies: 10's m for 100's Seconds

Met Office Approach: Unified Model (UM)



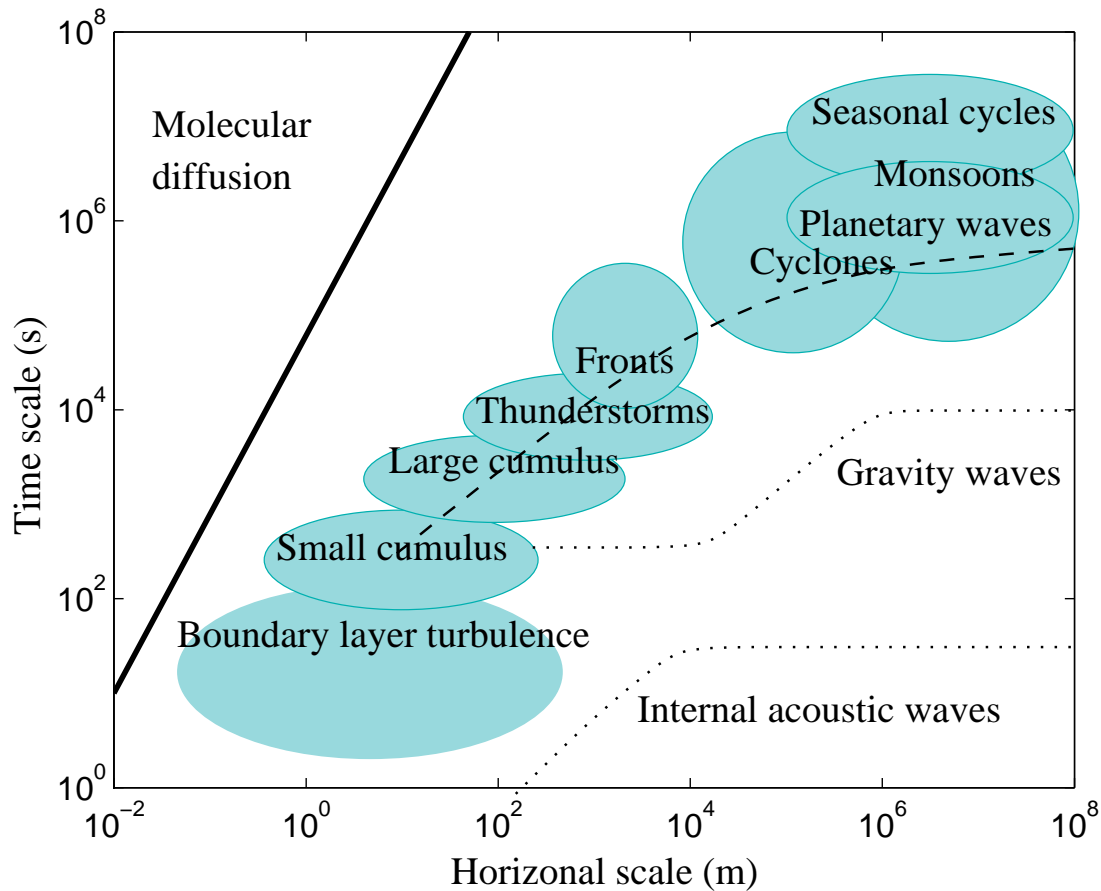
Forecast Constraints

Need to produce a forecast in a timely manner:

- Produce a forecast out to 7 days
- Global 10 km model, 70 vertical levels
- 4 Minute timestep \implies 2520 timesteps
- Resolution = $2560 \times 1920 \times 70 = 344$ million grid points per variable
- Fixed 1 Hour time window (Including data assimilation, model run and i/o)

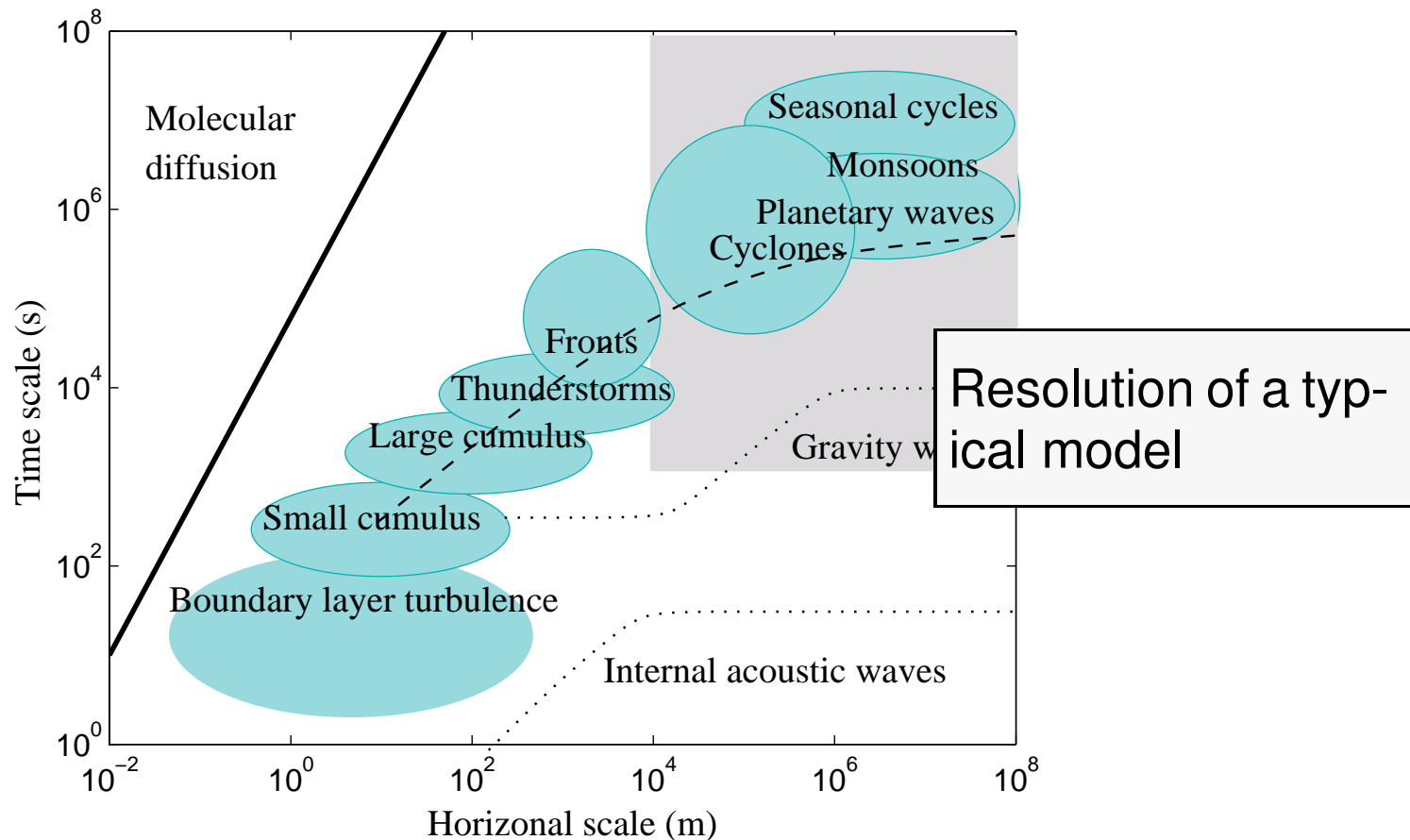
Algorithmic and code efficiency is critical

All Scales Problem



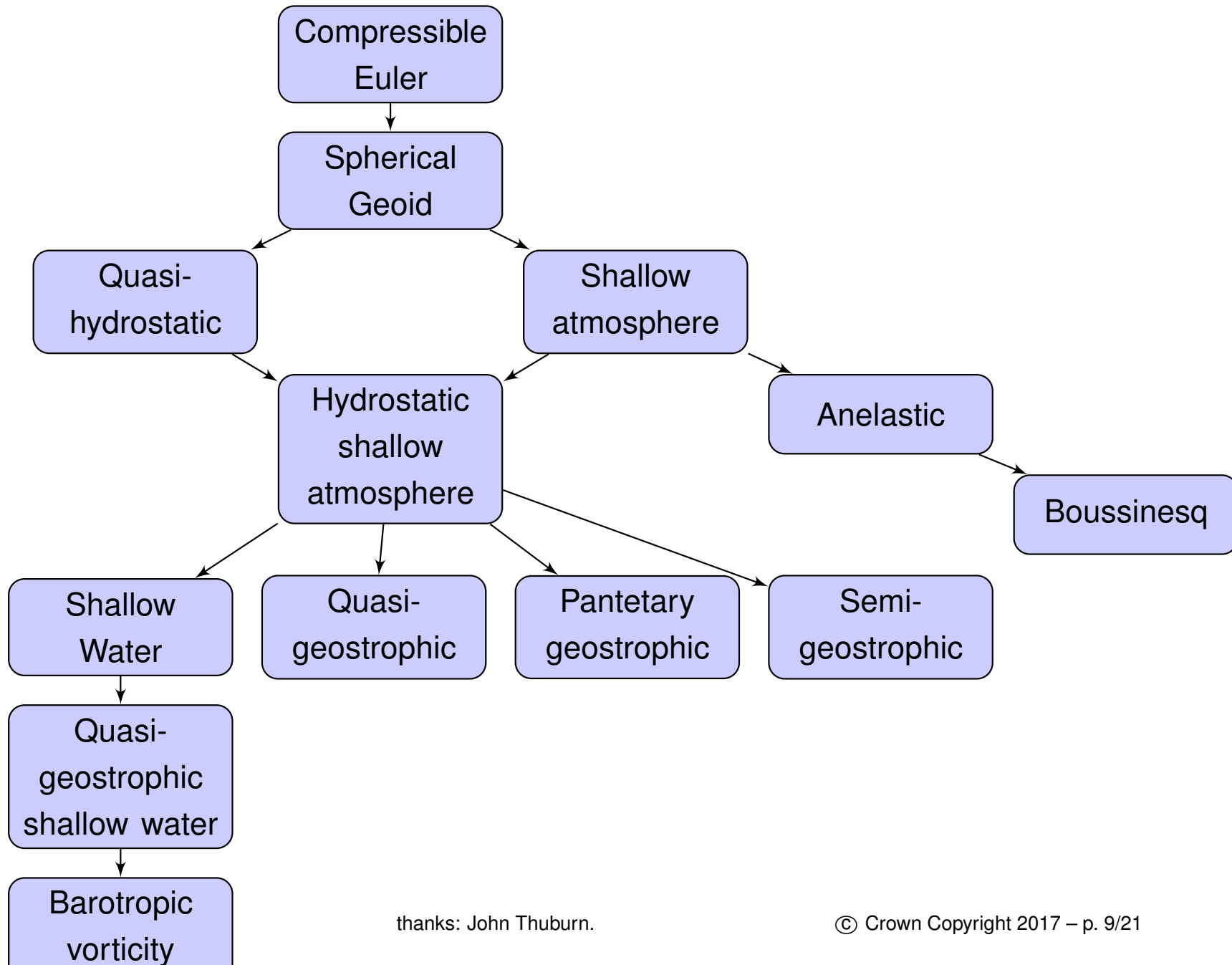
Phenomena occur across all time and space scales: No spectral gap

All Scales Problem



Phenomena occur across all time and space scales: No spectral gap

Dynamical Modelling: Equation Sets



Dynamical Core Modelling: 3D equations

Deep Atmosphere, nonhydrostatic equations: In spherical coordinates, this is the set that the Unified model uses. Only the spherical geoid approximation has been made.

$$\frac{D_r u}{Dt} - \frac{uv \tan \phi}{r} - 2\Omega \sin \phi v + \frac{c_{pd}\theta}{r \cos \phi} \frac{\partial \Pi}{\partial \lambda} = - \left(\frac{uw}{r} + 2\Omega \cos \phi w \right) + S^u$$

$$\frac{D_r v}{Dt} - \frac{u^2 \tan \phi}{r} + 2\Omega \sin \phi u + \frac{c_{pd}\theta}{r \cos \phi} \frac{\partial \Pi}{\partial \phi} = - \left(\frac{vw}{r} \right) + S^v$$

$$\frac{D_r w}{Dt} + c_{pd}\theta \frac{\partial \Pi}{\partial r} + \frac{\partial \Phi}{\partial r} = \frac{(u^2 + v^2)}{r} + 2\Omega \cos \phi u + S^w$$

$$\frac{D_r}{Dt} (\rho r^2 \cos \phi) + \rho r^2 \cos \phi \left(\frac{\partial}{\partial \lambda} \left[\frac{u}{r \cos \phi} \right] + \frac{\partial}{\partial \phi} \left[\frac{v}{r} \right] + \frac{\partial w}{\partial r} \right) = 0$$

$$\frac{D_r \theta}{Dt} = S^\theta$$

Dynamical Core Modelling: 3D equations

Shallow Atmosphere: Assume the atmosphere is a shallow shell. Replace height factors r with earth's radius a and neglect certain parts of the coriolis terms. Valid when $(r - a) \ll a$.

$$\frac{D_a u}{Dt} - \frac{uv \tan \phi}{a} - 2\Omega \sin \phi v + \frac{c_{pd}\theta}{a \cos \phi} \frac{\partial \Pi}{\partial \lambda} = - \left(\frac{uw}{r} + 2\Omega \cos \phi w \right) + S^u$$

$$\frac{D_a v}{Dt} - \frac{u^2 \tan \phi}{a} + 2\Omega \sin \phi u + \frac{c_{pd}\theta}{a \cos \phi} \frac{\partial \Pi}{\partial \phi} = - \left(\frac{vw}{r} \right) + S^v$$

$$\frac{D_a w}{Dt} + c_{pd}\theta \frac{\partial \Pi}{\partial r} + \frac{\partial \Phi}{\partial r} = \frac{(u^2 + v^2)}{r} + 2\Omega \cos \phi u + S^w$$

$$\frac{D_a}{Dt} (\rho a^2 \cos \phi) + \rho a^2 \cos \phi \left(\frac{\partial}{\partial \lambda} \left[\frac{u}{a \cos \phi} \right] + \frac{\partial}{\partial \phi} \left[\frac{v}{a} \right] + \frac{\partial w}{\partial r} \right) = 0$$

$$\frac{D_a \theta}{Dt} = S^\theta$$

Dynamical Core Modelling: 3D equations

Quasi-Hydrostatic: Neglect the vertical acceleration term Dw/Dt . This is a good approximation for horizontal scales greater than about $10km$. Filters out vertical acoustic waves

$$\frac{D_r u}{Dt} - \frac{uv \tan \phi}{r} - 2\Omega \sin \phi v + \frac{c_{pd}\theta}{r \cos \phi} \frac{\partial \Pi}{\partial \lambda} = - \left(\frac{uw}{r} + 2\Omega \cos \phi w \right) + S^u$$

$$\frac{D_r v}{Dt} - \frac{u^2 \tan \phi}{r} + 2\Omega \sin \phi u + \frac{c_{pd}\theta}{r \cos \phi} \frac{\partial \Pi}{\partial \phi} = - \left(\frac{vw}{r} \right) + S^v$$

$$\frac{D_r w}{Dt} + c_{pd}\theta \frac{\partial \Pi}{\partial r} + \frac{\partial \Phi}{\partial r} = \frac{(u^2 + v^2)}{r} + 2\Omega \cos \phi u + S^w$$

$$\frac{D_r}{Dt} (\rho r^2 \cos \phi) + \rho r^2 \cos \phi \left(\frac{\partial}{\partial \lambda} \left[\frac{u}{r \cos \phi} \right] + \frac{\partial}{\partial \phi} \left[\frac{v}{r} \right] + \frac{\partial w}{\partial r} \right) = 0$$

$$\frac{D_r \theta}{Dt} = S^\theta$$

Dynamical Core Modelling: 3D equations

Hydrostatic Shallow Atmosphere: Make the shallow atmosphere and hydrostatic approximations: Hydrostatic primitive equations. Historically popular for climate modelling

$$\frac{D_a u}{Dt} - \frac{uv \tan \phi}{a} - 2\Omega \sin \phi v + \frac{c_{pd}\theta}{a \cos \phi} \frac{\partial \Pi}{\partial \lambda} = - \left(\frac{uw}{r} + 2\Omega \cos \phi w \right) + S^u$$

$$\frac{D_r v}{Dt} - \frac{u^2 \tan \phi}{a} + 2\Omega \sin \phi u + \frac{c_{pd}\theta}{a \cos \phi} \frac{\partial \Pi}{\partial \phi} = - \left(\frac{vw}{r} \right) + S^v$$

$$\frac{D_a w}{Dt} + c_{pd}\theta \frac{\partial \Pi}{\partial r} + \frac{\partial \Phi}{\partial r} = \frac{(u^2 + v^2)}{r} + 2\Omega \cos \phi u + S^w$$

$$\frac{D_a}{Dt} (\rho a^2 \cos \phi) + \rho a^2 \cos \phi \left(\frac{\partial}{\partial \lambda} \left[\frac{u}{a \cos \phi} \right] + \frac{\partial}{\partial \phi} \left[\frac{v}{a} \right] + \frac{\partial w}{\partial r} \right) = 0$$

$$\frac{D_a \theta}{Dt} = S^\theta$$

Dynamical Core Modelling: Scaling

- Vertical momentum equation scalings:

<i>w</i> -equation	$\frac{Dw}{Dt}$	$-\frac{u^2+v^2}{r}$	$-2\Omega u \cos \phi$	$\frac{\partial \Phi}{\partial r}$	$\frac{1}{\rho} \frac{\partial p}{\partial r}$
Scales	UW/L	U^2/a	f_0U	g	$P_0/\rho H$
Values (<i>m/s</i>)	10^{-7}	10^{-5}	10^{-3}	10	10

- Horizontal momentum equation scalings:

<i>u</i> -equation	$\frac{Du}{Dt}$	$-\frac{uv \tan \phi}{r}$	$\frac{uw}{r}$	$-2\Omega v \sin \phi$	$2\Omega w \cos \phi$	$\frac{1}{\rho r \cos \phi} \frac{\partial p}{\partial \lambda}$
<i>v</i> -equation	$\frac{Dv}{Dt}$	$-\frac{u^2 \tan \phi}{r}$	$\frac{vw}{r}$	$-2\Omega u \sin \phi$		$\frac{1}{\rho r} \frac{\partial p}{\partial \phi}$
Scales	U^2/L	U^2/a	UW/a	f_0U	f_0W	$\delta P/\rho L$
Values (<i>m/s</i>)	10^{-4}	10^{-5}	10^{-8}	10^{-3}	10^{-6}	10^{-3}

Dynamical Core Modelling: Geostrophic approximations

Geostrophic: Coriolis force (f) balances the pressure gradient (∇p)

$$\mathbf{v}_G = \frac{1}{\rho f} \mathbf{k} \times \nabla_h p$$

Valid for small Rossby numbers $R_0 \equiv \frac{V}{fL} \ll 1$

Dynamical Core Modelling: Geostrophic approximations

Geostrophic: Coriolis force (f) balances the pressure gradient (∇p)

$$\mathbf{v}_G = \frac{1}{\rho f} \mathbf{k} \times \nabla_h p$$

Valid for small Rossby numbers $R_0 \equiv \frac{V}{fL} \ll 1$

Quasi-geostrophic: Assume Cartesian geometry with a constant Coriolis force f_0 in geostrophic wind and include ageostrophic component: $\mathbf{v} = \mathbf{v}_a + \mathbf{v}_G$, $\mathbf{v}_a \ll \mathbf{v}_G$. Valid for flows with $L \ll a$ and small perturbations around reference depth

Dynamical Core Modelling: Geostrophic approximations

Geostrophic: Coriolis force (f) balances the pressure gradient (∇p)

$$\mathbf{v}_G = \frac{1}{\rho f} \mathbf{k} \times \nabla_h p$$

Valid for small Rossby numbers $R_0 \equiv \frac{V}{fL} \ll 1$

Quasi-geostrophic: Assume Cartesian geometry with a constant Coriolis force f_0 in geostrophic wind and include ageostrophic component: $\mathbf{v} = \mathbf{v}_a + \mathbf{v}_G$, $\mathbf{v}_a \ll \mathbf{v}_G$. Valid for flows with $L \ll a$ and small perturbations around reference depth

Planetary geostrophic: Retain the spherical geometry, valid for $L \approx a$

Dynamical Core Modelling: Geostrophic approximations

Geostrophic: Coriolis force (f) balances the pressure gradient (∇p)

$$\mathbf{v}_G = \frac{1}{\rho f} \mathbf{k} \times \nabla_h p$$

Valid for small Rossby numbers $R_0 \equiv \frac{V}{fL} \ll 1$

Quasi-geostrophic: Assume Cartesian geometry with a constant Coriolis force f_0 in geostrophic wind and include ageostrophic component: $\mathbf{v} = \mathbf{v}_a + \mathbf{v}_G$, $\mathbf{v}_a \ll \mathbf{v}_G$. Valid for flows with $L \ll a$ and small perturbations around reference depth

Planetary geostrophic: Retain the spherical geometry, valid for $L \approx a$

Semi-geostrophic: Assume Cartesian geometry. Use the full wind in the advection terms. Only drop the advection of the ageostrophic component: $D\mathbf{v}_a/Dt = 0$

Dynamical Core Modelling: Shallow water approximations

Shallow Water Equations: Neglect variations with height, assume the fluid is a single layer and the wavelength λ of surface waves is much smaller than fluid depth $\lambda \ll d$.

$$\frac{D\mathbf{u}}{Dt} = -2\boldsymbol{\Omega} \times \mathbf{u} - \nabla (\Phi + \Phi_0) = 0,$$

$$\frac{\partial \Phi}{\partial t} + \nabla \cdot (\Phi \mathbf{u}) = 0.$$

useful for testing numerical approximations in a simplified environment.

Dynamical Core Modelling: Shallow water approximations

Shallow Water Equations: Neglect variations with height, assume the fluid is a single layer and the wavelength λ of surface waves is much smaller than fluid depth $\lambda \ll d$.

$$\frac{D\mathbf{u}}{Dt} = -2\Omega \times \mathbf{u} - \nabla(\Phi + \Phi_0) = 0,$$

$$\frac{\partial\Phi}{\partial t} + \nabla \cdot (\Phi\mathbf{u}) = 0.$$

useful for testing numerical approximations in a simplified environment.

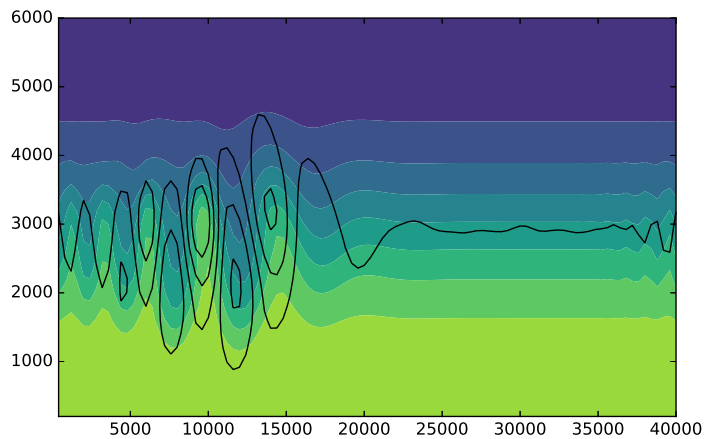
Barotropic vorticity: Describes incompressible 2D flow,

$$\frac{D\xi}{Dt} = 0,$$

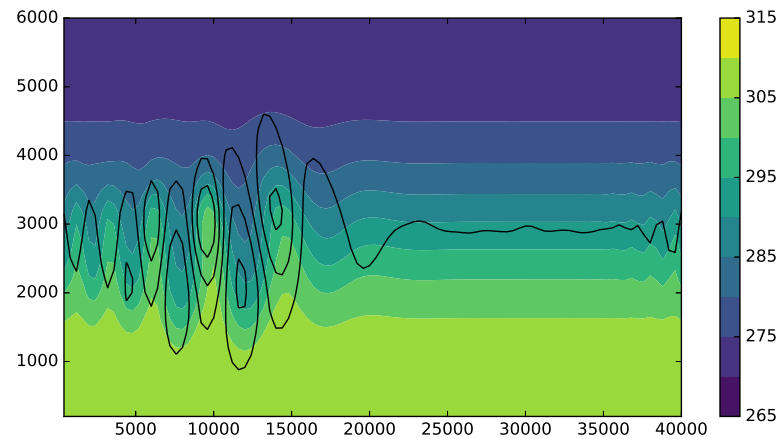
$$\mathbf{u} = \nabla^\perp \psi, \quad \nabla^2 \psi = \xi.$$

Dynamical Core Modelling: Effects of approximations

Baroclinic wave test case. Standard test for development of mid latitude weather systems



Unapproximated model



Hydrostatic approximation

Dynamical Modelling: Design Factors

Staniforth & Thuburn (QJRMS **138**, 2012) identified ten *Essential and desirable properties of a dynamical core*

- 1 Mass conservation
- 2 Accurate representation of balance and adjustment
- 3 Absence of, or well controlled, computational modes
Requires, at least, #velocity = 2x#pressure points

Dynamical Modelling: Design Factors

Staniforth & Thuburn (QJRMS **138**, 2012) identified ten *Essential and desirable properties of a dynamical core*

4 Geopotential and pressure gradient should not produce unphysical vorticity

$$\nabla \times (\nabla p) = 0$$

5 Energy conserving pressure terms

$$\mathbf{u} \cdot \nabla p + p \nabla \cdot \mathbf{u} = \nabla \cdot (\mathbf{u} p)$$

6 Energy conserving Coriolis terms

$$\mathbf{u} \cdot (\boldsymbol{\Omega} \times \mathbf{u}) = 0$$

7 No spurious fast propagation of Rossby modes

8 Axial angular momentum should be conserved

These all relate to the mimetic (compatible) properties of the numerics

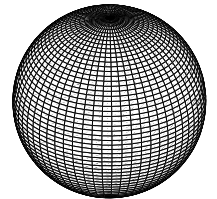
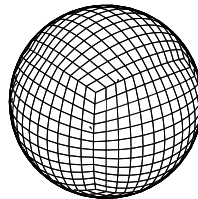
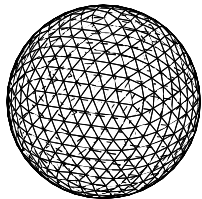
Dynamical Modelling: Design Factors

Staniforth & Thuburn (QJRMS **138**, 2012) identified ten *Essential and desirable properties of a dynamical core*

9 Accuracy at least approaching second order

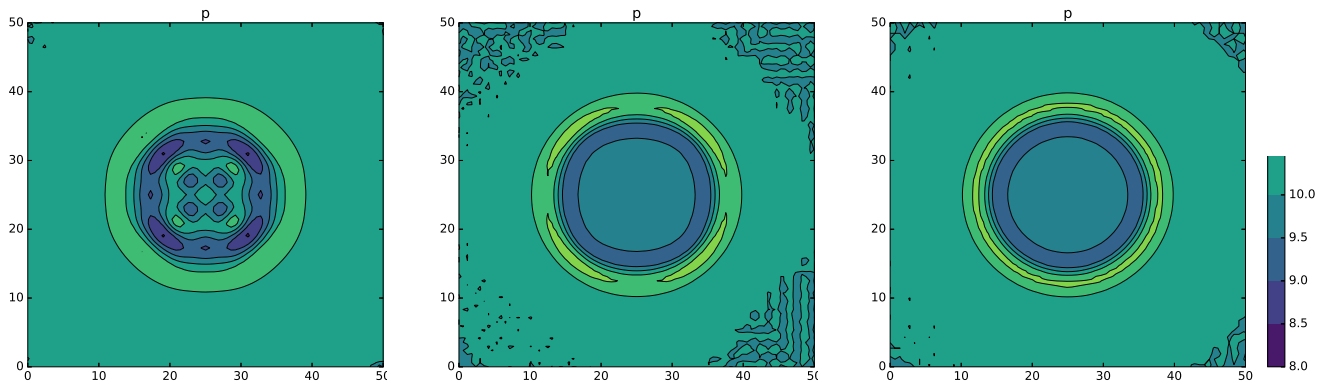
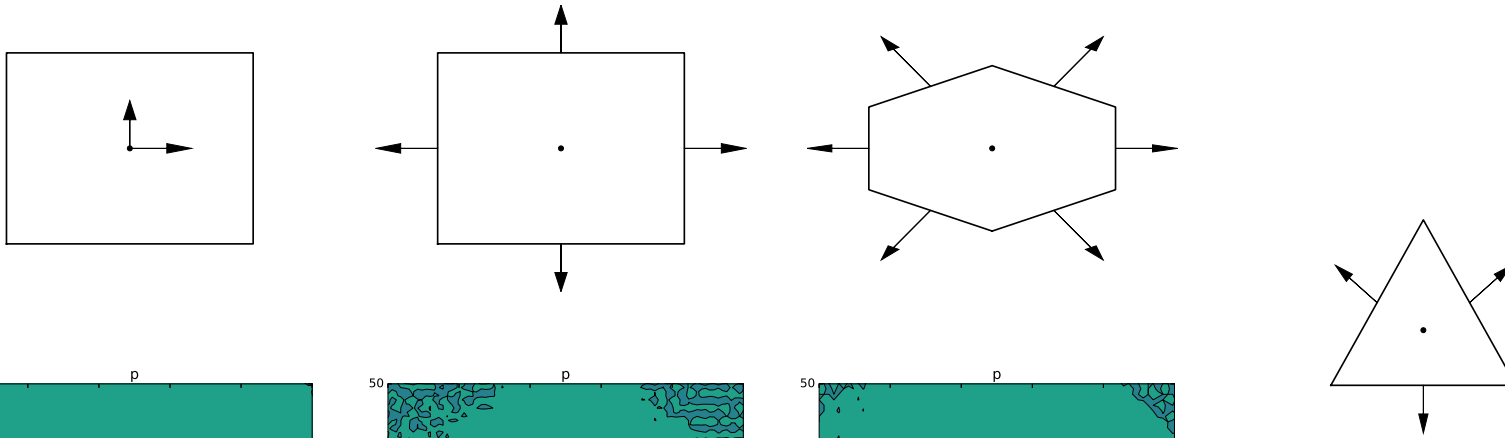
10 Minimal grid imprinting

*These are challenging for grids with special points
...generally require higher order schemes*



Representation of fast waves

Linear shallow water model in a Cartesian domain



Mixed finite element model

Developing a new model based suitable for future supercomputers

- Using mixed finite-element method
- Choose finite element function space to give discrete De-Rahm complex

$$\begin{array}{ccccccc} H_1 & & H_{curl} & & H_{div} & & L_2 \\ & \nabla & & \nabla \times & & \nabla \cdot & \\ \mathbb{W}_0 & \longrightarrow & \mathbb{W}_1 & \longrightarrow & \mathbb{W}_2 & \longrightarrow & \mathbb{W}_3 \end{array}$$

Mixed finite element model

Developing a new model based suitable for future supercomputers

- Using mixed finite-element method
- Choose finite element function space to give discrete De-Rahm complex

$$\begin{array}{ccccccc} H_1 & & H_{curl} & & H_{div} & & L_2 \\ & \nabla & & \nabla \times & & \nabla \cdot & \\ W_0 & \longrightarrow & W_1 & \longrightarrow & W_2 & \longrightarrow & W_3 \\ Q_{k+1} & & N_k & & RT_k & & Q_k^{DG} \end{array}$$

Mixed finite element model

Developing a new model based suitable for future supercomputers

- Using mixed finite-element method
- Choose finite element function space to give discrete De-Rahm complex

$$\begin{array}{ccccccc} & H_1 & & H_{curl} & & H_{div} & & L_2 \\ & & \nabla & & \nabla \times & & \nabla \cdot & \\ \mathbb{W}_0 & \longrightarrow & \mathbb{W}_1 & \longrightarrow & \mathbb{W}_2 & \longrightarrow & \mathbb{W}_3 & \end{array}$$

- Accurate for arbitrary grids, (no orthogonality constraint)
- Flexibility to increase formal order of accuracy
- Builds in mimetic and conservation properties
- Generalises staggered grid finite-volume methods

Timestepping

Two main approaches used:

- Explicit
- Semi-Implicit

Timestepping

Explicit timestepping (e.g. Runge-Kutta) is simple and cheap per step but restricted by speed of fast (acoustic & inertia-gravity waves)

- Explicit in the vertical: $U \approx 340m/s$, $\Delta z \approx 10m$ leads to $\Delta t < 1/4s$
- Only explicit in the horizontal: $U \approx 340m/s$, $\Delta x \approx 10Km$ leads to $\Delta t < 30s$
- Alternatively try to filter fast waves (hydrostatic, anelastic approximations)

Timestepping

Implicit timestepping is more complex and expensive per step but much longer timestep can be taken

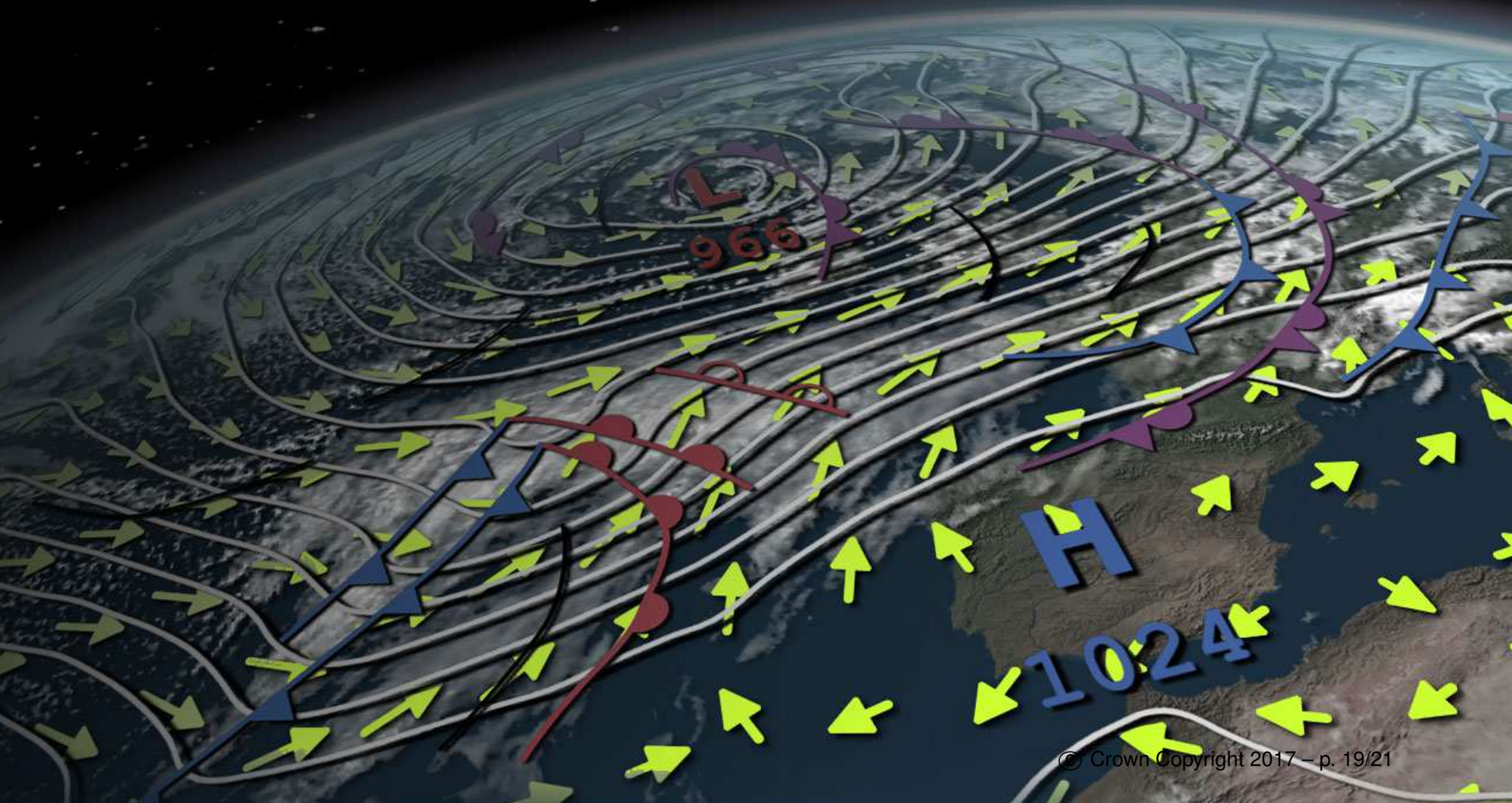
- UM uses ≈ 5 minutes for $\Delta x = 10Km$
- Forming full Jacobian for Newton method is expensive
- More common to use Quasi-Newton (semi-implicit) method

$$\begin{pmatrix} 1 & \tau \Delta t \nabla \Pi^* & 0 & \tau \Delta t \theta^* \nabla \\ \tau \Delta t \nabla \theta^* & 1 & 0 & 0 \\ \nabla \cdot \rho^* & 0 & 1 & 0 \\ 0 & \frac{1}{\theta} & \frac{1}{\rho^*} & \frac{\gamma}{\Pi^*} \end{pmatrix} \begin{pmatrix} \mathbf{u}' \\ \theta' \\ \rho' \\ \Pi' \end{pmatrix} = R$$

- Only the terms for fast waves are retained
- Usually use Schur complement to reduce this to a single (Helmholtz) equation

$$H(\Pi') \equiv \alpha_1 \Pi' + \alpha_2 \nabla \cdot (\alpha_3 \nabla [\alpha_4 \Pi']) = RHS$$

Any Questions?



Atmospheric Model Splitting

Atmospheric model is split into two main parts

- Dynamical Core: Models all motions that are resolved on the mesh
- Physical Parameterisations: Models subgrid processes that are not resolved

Dynamical Core:

- Solves equations of motion
- Transport of fields
- Resolves large scale balances



Atmospheric Model Splitting

Atmospheric model is split into two main parts

- Dynamical Core: Models all motions that are resolved on the mesh
- Physical Parameterisations: Models subgrid processes that are not resolved

Physical Parameterisations:

- Deep & shallow convection
- Microphysics
- Radiation
- Boundary layer
- Gravity wave drag



Atmospheric Model Splitting

Atmospheric model is split into two main parts

- Dynamical Core: Models all motions that are resolved on the mesh
- Physical Parameterisations: Models subgrid processes that are not resolved

Dynamical Core:

- Solves equations of motion
- Transport of fields
- Resolves large scale balances



Atmospheric Model Splitting

Atmospheric model is split into two main parts

- Dynamical Core: Models all motions that are resolved on the mesh
- Physical Parameterisations: Models subgrid processes that are not resolved

Physical Parameterisations:

- Deep & shallow convection
- Microphysics
- Radiation
- Boundary layer
- Gravity wave drag

