Transported Probability Density Function (PDF) Methods for Multiscale and Uncertainty Problems - Part III

A Solution Algorithm for the Fluid Dynamic Equations Based on a Stochastic Model for Molecular Motion (cont.)

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Fokker-Planck Solution Algorithm

$$\frac{\partial \mathcal{F}}{\partial t} + V_i \frac{\partial \mathcal{F}}{\partial x_i} + \frac{\partial F_i \mathcal{F}}{\partial V_i} = S^{(FP)}(\mathcal{F}) = \frac{\partial}{\partial V_i} \left(\frac{1}{\tau_{FP}} (V_i - U_i) \mathcal{F} \right) + \frac{\partial^2}{\partial V_k \partial V_k} \left(\frac{2e_s}{3\tau_{FP}} \mathcal{F} \right)$$

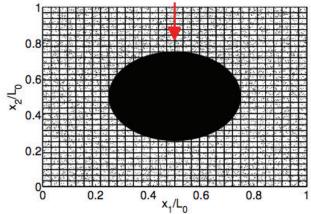
solved through stochastic motion of notional particles

$$rac{dX_i}{dt} = M_i \quad ext{with}$$
 $rac{dM_i}{dt} = -rac{1}{ au}\left(M_i - U_i\right) + \left(rac{4e_s}{3 au}
ight)^{1/2}rac{dW_i(t)}{dt} + F_i$

Fokker-Planck Solution Algorithm

 n_t time steps are performed

- (1) U and e_s at time t are estimated at each grid node and interpolated to the particle positions,
- (2) the time step size Δt is determined,
- (3) a first half-step is performed to estimate the particle mid-points,
- (4) mid-point boundary conditions are applied,
- (5) U and e_s at time $t + \Delta t/2$ are interpolated from the grid nodes to the particle mid-point positions,
- (6) the new particle velocities and positions are computed, and
- (7) the boundary conditions are enforced.



in statistical steady state U and e_s do not depend on the time

Estimation of Statistical Moments

$$\mathcal{U}^{J}(t) =$$

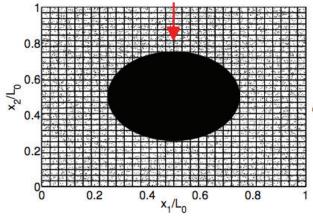
$$\mathcal{E}^J(t) =$$

$$\mathcal{W}^J(t) =$$

$$\sum_{j=1}^{N_p} \left\{ \hat{g}^J(oldsymbol{X}^j(t)) oldsymbol{M}^j(t)
ight\},$$

$$\sum_{j=1}^{N_p} \left\{ \hat{g}^J(oldsymbol{X}^j(t)) oldsymbol{M}^j(t) \cdot oldsymbol{M}^j(t)
ight\}$$

$$\sum_{j=1}^{N_p} \left\{ \hat{g}^J(oldsymbol{X}^j(t))
ight\},$$

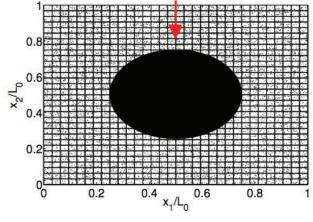


$$oldsymbol{U}(oldsymbol{x}^J,t)\!=\!rac{\mathcal{U}^J(t)}{\mathcal{W}^J(t)}$$

$$oldsymbol{e}_{s}(oldsymbol{x}^{J},t) = rac{1}{2} \left(rac{\mathcal{E}^{J}(t)}{\mathcal{W}^{J}(t)} \ - \ oldsymbol{U}^{J}(t) \cdot oldsymbol{U}^{J}(t)
ight)$$

Estimation of Statistical Moments

$$\mathcal{U}^J(t) = \mu \mathcal{U}^J(t - \Delta t) + (1 - \mu) \sum_{j=1}^{N_p} \left\{ \hat{g}^J(\boldsymbol{X}^j(t)) \boldsymbol{M}^j(t) \right\},$$
 $\mathcal{E}^J(t) = \mu \mathcal{E}^J(t - \Delta t) + (1 - \mu) \sum_{j=1}^{N_p} \left\{ \hat{g}^J(\boldsymbol{X}^j(t)) \boldsymbol{M}^j(t) \cdot \boldsymbol{M}^j(t) \right\}$ $\mathcal{W}^J(t) = \mu \mathcal{W}^J(t - \Delta t) + (1 - \mu) \sum_{j=1}^{N_p} \left\{ \hat{g}^J(\boldsymbol{X}^j(t)) \right\},$

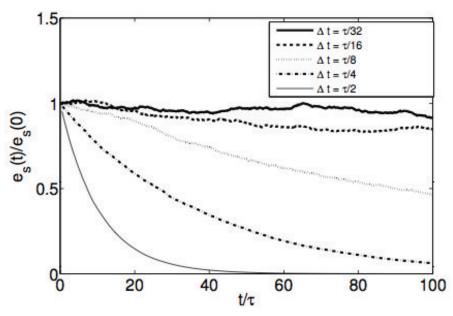


$$oldsymbol{U}(oldsymbol{x}^J,t) = rac{\mathcal{U}^J(t)}{\mathcal{W}^J(t)}$$

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ight)$$

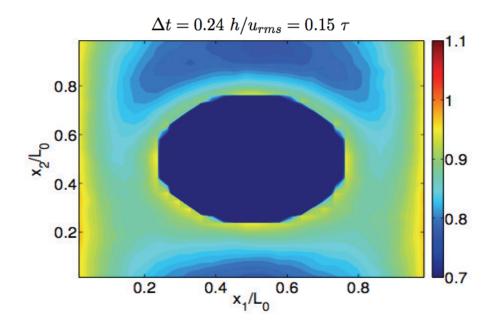
Particle Evolution

$$rac{dX_i}{dt} = M_i \quad ext{with}$$
 $rac{dM_i}{dt} = -rac{1}{ au}\left(M_i - U_i
ight) + \left(rac{4e_s}{3 au}
ight)^{1/2}rac{dW_i(t)}{dt} + F_i$



$$M_i^{n+1} - M_i^n = \left[-\frac{\Delta t}{\tau} M_i^n + \left(\frac{4e_s}{3\tau} \Delta t \right)^{1/2} \xi_i \right] \left[1 - \frac{\Delta t}{2\tau} \right]$$
 and $\Delta X_i^{n+1} = \frac{\Delta t}{2} \left(M_i^n + M_i^{n+1} \right)$

Particle Evolution



$$M_i^{n+1} - M_i^n = \left[-\frac{\Delta t}{\tau} M_i^n + \left(\frac{4e_s}{3\tau} \Delta t \right)^{1/2} \xi_i \right] \left[1 - \frac{\Delta t}{2\tau} \right] \quad \text{and}$$

$$\Delta X_i^{n+1} = \frac{\Delta t}{2} \left(M_i^n + M_i^{n+1} \right)$$

(up to 2nd moments)

statistically exact for constant U and e_s for any time step Δt : without loss of generality, $U_i = F_i = 0$ is assumed

solution of
$$\frac{dX_i}{dt} = M_i$$
 and $\frac{dM_i}{dt} = -\frac{1}{\tau}M_i + \left(\frac{4e_s}{3\tau}\right)^{1/2}\frac{dW_i(t)}{dt}$ is considered

$$M_i^{n+1} = M_i^n e^{-\Delta t/\tau} + \lim_{N \to \infty} \sum_{k=1}^N \xi_{k,i} \left(\frac{4e_s}{3\tau} \frac{\Delta t}{N} \right)^{1/2} e^{-k\Delta t/(N\tau)}$$

 $\xi_{k,i}$ are independent, normal distributed random variables leads to the conditional expectation $\left\langle M_i^{n+1}M_j^{n+1}\middle|M^n\right\rangle=M_i^nM_j^ne^{-2\Delta t/\tau}+\delta_{ij}\lim_{N\to\infty}\sum_{k=1}^N\frac{4e_s}{3\tau}\frac{\Delta t}{N}e^{-2k\Delta t/(N\tau)}$ cross products disappear, since $\langle \xi_{k,i}\xi_{h,j}\rangle=\delta_{kh}\delta_{ij}$ and $\langle \xi_{k,i}\rangle=0$

(up to 2nd moments)

statistically exact for constant U and e_s for any time step Δt : without loss of generality, $U_i = F_i = 0$ is assumed

solution of
$$\frac{dX_i}{dt} = M_i$$
 and $\frac{dM_i}{dt} = -\frac{1}{\tau}M_i + \left(\frac{4e_s}{3\tau}\right)^{1/2}\frac{dW_i(t)}{dt}$ is considered

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$$\left\langle M_i^{n+1} M_j^{n+1} \middle| \mathbf{M}^n \right\rangle = M_i^n M_j^n e^{-2\Delta t/\tau} + \delta_{ij} \frac{4e_s}{3\tau} \int_0^{\Delta t} e^{-2t/\tau} dt$$

$$= M_i^n M_j^n e^{-2\Delta t/\tau} + \delta_{ij} \frac{2e_s}{3} \left(1 - e^{-2\Delta t/\tau} \right)$$

therefore
$$M_i^{n+1} = M_i^n e^{-\Delta t/\tau} + \left(\frac{2e_s}{3} \left(1 - e^{-2\Delta t/\tau}\right)\right)^{1/2} \xi_{M,i}$$

$$M_i^{n+1} = M_i^n e^{-\Delta t/ au} + \left(\frac{2e_s}{3} \left(1 - e^{-2\Delta t/ au}\right)\right)^{1/2} \xi_{M,i}$$

preserves the internal energy $e_s = \frac{\langle M_i^n M_i^n \rangle}{2}$ independent of the time step size Δt

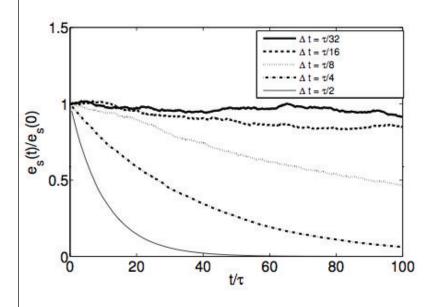
$$\begin{split} \langle M_i^{n+1} M_i^{n+1} \rangle &= \langle M_i^n M_i^n \rangle e^{-2\Delta t/\tau} + 2e_s \left(1 - e^{-2\Delta t/\tau} \right) \\ &= \left(\langle M_i^n M_i^n \rangle - 2e_s \right) e^{-2\Delta t/\tau} + 2e_s, \end{split}$$

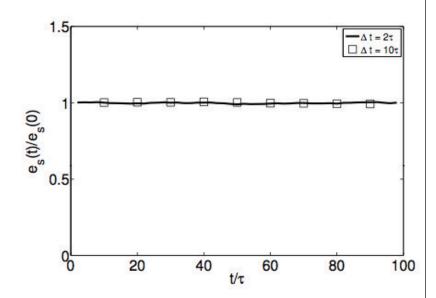
analytically correct correlation coefficient

$$\frac{\langle M_i^{n+1} M_i^n \rangle}{\langle M_i^n M_i^n \rangle} = e^{-\Delta t/\tau}$$

Validation of the Exact Scheme

internal energy:





$$egin{align} rac{dX_i}{dt} = M_i \quad ext{and} \ rac{dM_i}{dt} = -rac{1}{ au}M_i + \left(rac{4e_s}{3 au}
ight)^{1/2}rac{dW_i(t)}{dt} \ \end{aligned}$$

exact particle position scheme

$$\Delta X_{i}^{n+1} = X_{i}^{n+1} - X_{i}^{n} = M_{i}^{n} \tau \left(1 - e^{-\Delta t/\tau} \right)$$

$$+ \lim_{N \to \infty} \sum_{k=1}^{N} \xi_{k,i} \left(\frac{4e_{s}}{3\tau} \frac{\Delta t}{N} \right)^{1/2} \tau \left(1 - e^{-k\Delta t/(N\tau)} \right)$$

$$\begin{split} \left\langle \Delta X_i^{n+1} \Delta X_j^{n+1} \middle| \boldsymbol{M}^n \right\rangle &= M_i^n M_j^n \tau^2 \left(1 - e^{-\Delta t/\tau} \right)^2 \\ &+ \delta_{ij} \lim_{N \to \infty} \sum_{k=1}^N \frac{4e_s}{3\tau} \frac{\Delta t}{N} \tau^2 \left(1 - e^{-k\Delta t/(N\tau)} \right)^2 \end{split}$$

$$\left\langle \Delta X_i^{n+1} \Delta X_j^{n+1} \middle| \mathbf{M}^n \right\rangle = M_i^n M_j^n \tau^2 \left(1 - e^{-\Delta t/\tau} \right)^2$$

$$+ \delta_{ij} \lim_{N \to \infty} \sum_{k=1}^N \frac{4e_s}{3\tau} \frac{\Delta t}{N} \tau^2 \left(1 - e^{-k\Delta t/(N\tau)} \right)^2$$

which can be written as

$$\begin{split} \left\langle \Delta X_i^{n+1} \Delta X_j^{n+1} \middle| \boldsymbol{M}^n \right\rangle &= M_i^n M_j^n \tau^2 \left(1 - e^{-\Delta t/\tau} \right)^2 \\ &+ \delta_{ij} \frac{4e_s}{3} \tau \int_0^{\Delta t} \left(1 - 2e^{-t/\tau} + e^{-2t/\tau} \right) dt \\ &= M_i^n M_j^n \tau^2 \left(1 - e^{-\Delta t/\tau} \right)^2 \\ &+ \delta_{ij} \frac{2e_s \tau^2}{3} \left(\frac{2\Delta t}{\tau} - \left(1 - e^{-\Delta t/\tau} \right) \left(3 - e^{-\Delta t/\tau} \right) \right) \end{split}$$

$$\Delta X_i^{n+1} = M_i^n \tau \left(1 - e^{-\Delta t/\tau} \right)$$

$$+\left(rac{2e_s au^2}{3}\left(rac{2\Delta t}{ au}-\left(1-e^{-\Delta t/ au}
ight)\left(3-e^{-\Delta t/ au}
ight)
ight)^{1/2}\xi_{X,i}$$

$$M_i^{n+1} = M_i^n e^{-\Delta t/\tau} + \lim_{N \to \infty} \sum_{k=1}^N \xi_{k,i} \left(\frac{4e_s}{3\tau} \frac{\Delta t}{N} \right)^{1/2} e^{-k\Delta t/(N\tau)}$$

$$\begin{split} \Delta X_i^{n+1} \; &= \; X_i^{n+1} - X_i^n = M_i^n \tau \left(1 - e^{-\Delta t/\tau} \right) \\ &+ \lim_{N \to \infty} \sum_{k=1}^N \xi_{k,i} \Big(\frac{4e_s}{3\tau} \frac{\Delta t}{N} \Big)^{1/2} \tau \left(1 - e^{-k\Delta t/(N\tau)} \right) \end{split}$$

$$\begin{split} \left\langle M_{i}^{n+1} \Delta X_{j}^{n+1} \middle| M^{n} \right\rangle &= M_{i}^{n} M_{j}^{n} \tau \left(e^{-\Delta t/\tau} - e^{-2\Delta t/\tau} \right) \\ &+ \delta_{ij} \lim_{N \to \infty} \sum_{k=1}^{N} \frac{4e_{s}}{3\tau} \frac{\Delta t}{N} \tau \left(e^{-k\Delta t/(N\tau)} - e^{-2k\Delta t/(N\tau)} \right) \\ &= M_{i}^{n} M_{j}^{n} \tau \left(e^{-\Delta t/\tau} - e^{-2\Delta t/\tau} \right) \\ &+ \delta_{ij} \frac{4e_{s}}{3} \int_{0}^{\Delta t} \left(e^{-t/\tau} - e^{-2t/\tau} \right) dt \\ &= M_{i}^{n} M_{j}^{n} \tau \left(e^{-\Delta t/\tau} - e^{-2\Delta t/\tau} \right) \\ &+ \delta_{ij} \underbrace{\frac{2e_{s}\tau}{3} \left(1 - e^{-\Delta t/\tau} \right)^{2}}_{C}. \end{split}$$

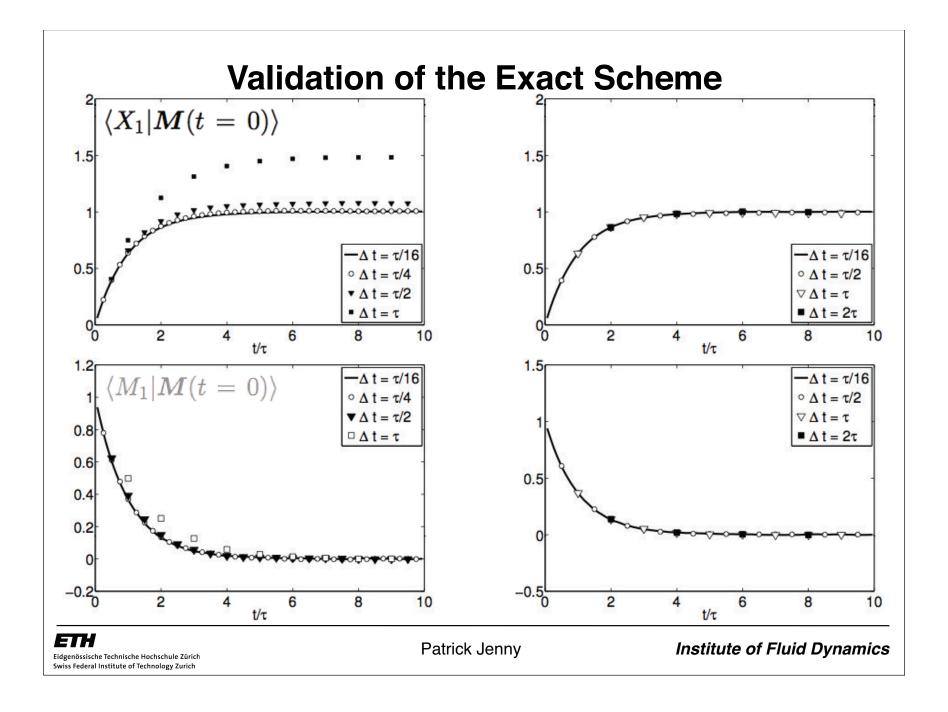
$$M_i^{n+1} = M_i^n e^{-\Delta t/\tau} + \underbrace{\left(\frac{2e_s}{3} \left(1 - e^{-2\Delta t/\tau} \right) \right)^{1/2}}_{A} \xi_{M,i}$$

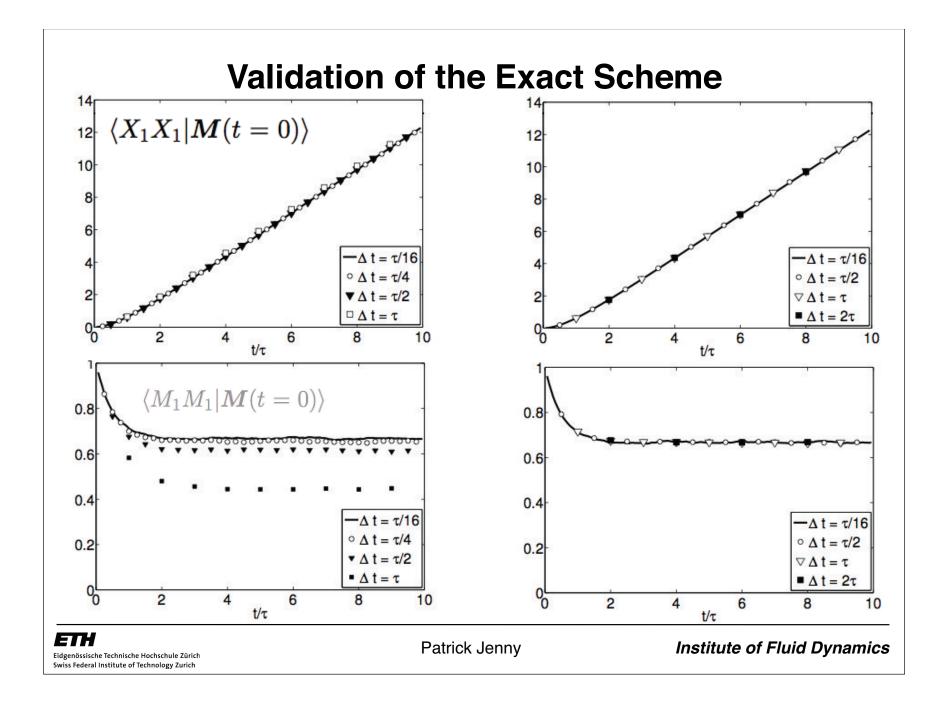
$$\Delta X_i^{n+1} = M_i^n \tau \left(1 - e^{-\Delta t/\tau}\right)$$

$$+ \underbrace{\left(\frac{2e_s \tau^2}{3} \left(\frac{2\Delta t}{\tau} - \left(1 - e^{-\Delta t/\tau}\right) \left(3 - e^{-\Delta t/\tau}\right)\right)\right)^{1/2}}_{B} \xi_{X,i}$$

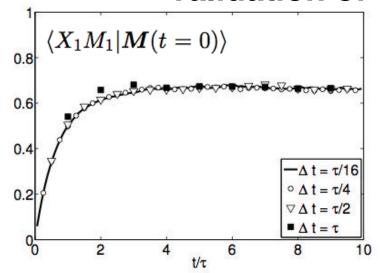
$$S'_{M,i} = \left(\frac{C^2}{B}\right)^{1/2} \xi_{1,i} + \left(A - \frac{C^2}{B}\right)^{1/2} \xi_{2,i}$$
 and $S'_{X,i} = (B)^{1/2} \xi_{1,i}$,

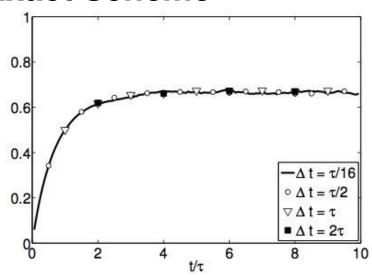
$$\langle S'_{M,i}S'_{M,j}\rangle = \langle S_{M,i}S_{M,j}\rangle = \delta_{ij}A$$
 and $\langle S'_{X,i}S'_{X,j}\rangle = \langle S_{X,i}S_{X,j}\rangle = \delta_{ij}B,$ $\langle S'_{M,i}S'_{X,j}\rangle = C$





Validation of the Exact Scheme

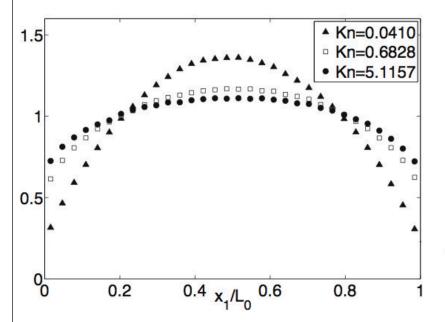


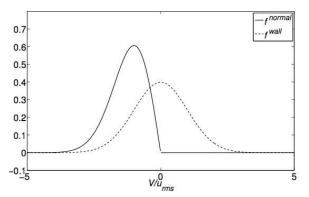


Knudsen Paradox

Periodic-, open- and wall boundary conditions

isothermal wall is treated as an interface between computational and a virtual domain





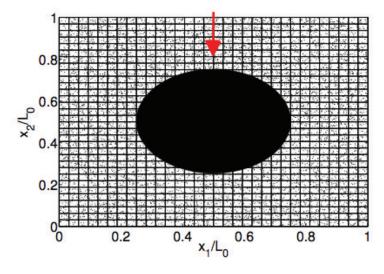
$$f^{wall} = \frac{1}{(2\pi k T^{wall}/m)^{1/2}} \exp\left(-\frac{V_i^2}{2k T^{wall}/m}\right)$$

$$f^{normal} = \frac{-H(-V_n)V_n}{Q} \frac{1}{(2\pi k T^{wall}/m)^{1/2}} \exp\left(-\frac{V_n^2}{2k T^{wall}/m}\right)$$

Flow Around a Cylinder

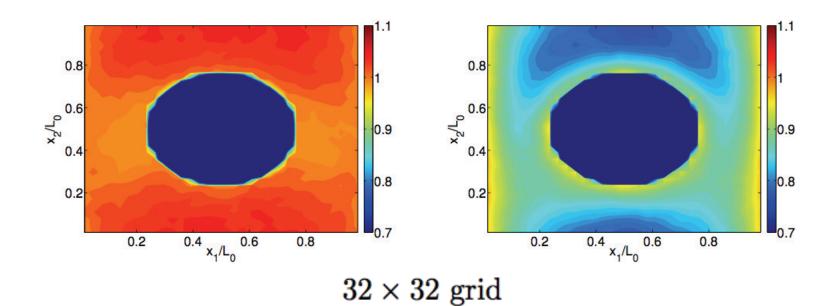
$$Kn = \lambda/(0.25L_0) = 2\sqrt{RT^{wall}}\tau/L_0 = 0.1$$

 $\hat{F} = FL_0/(RT^{wall}) = 0.4$



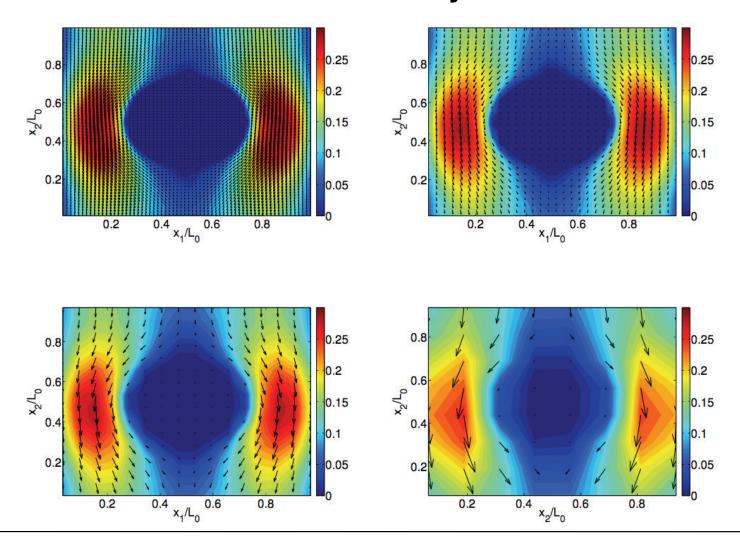
 64×64 , 32×32 , 16×16 and 8×8 grids 10 particles / cell averaging factor n_a of 10'000 $\Delta t = 0.24 h/u_{rms}$

Flow Around a Cylinder



 $\Delta t = 0.24~h/u_{rms} = 0.15~\tau$

Flow Around a Cylinder

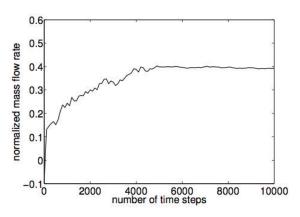


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Performance

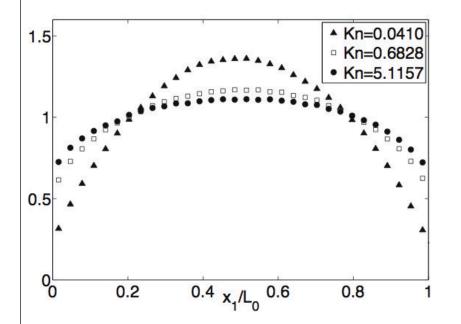


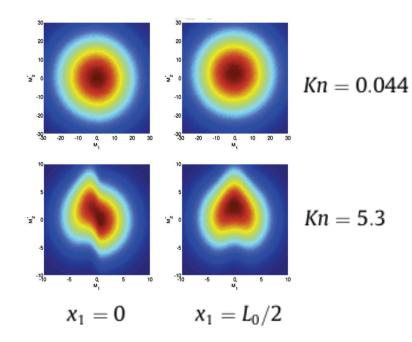
Knudsen paradox (Kn=5.1157):
$$\frac{\partial \mathcal{F}}{\partial t} + V_i \frac{\partial \mathcal{F}}{\partial x_i} + \frac{\partial}{\partial V_i} \left\{ \left[F_i - \frac{1}{\tau} \left(V_i - U_i \right) \right] \mathcal{F} \right\} = \frac{\partial^2}{\partial V_i \partial V_i} \left\{ \frac{2e_s}{3\tau} \mathcal{F} \right\}$$

number of grid cells	\hat{J}/\hat{F}	number of grid cells	Δt	\hat{J}/\hat{F}
64	1.315	64×64	0.075τ	0.368653
32	1.317	32 imes 32	0.15 au	0.378591
16	1.327	16 imes 16	0.3τ	0.385789
8	1.341	8×8	0.6 au	0.387631
4	1.383			

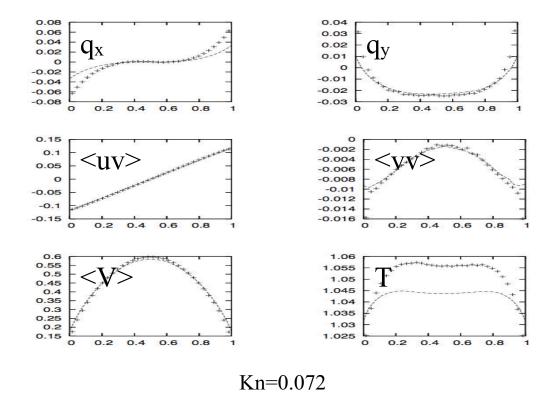
ETH

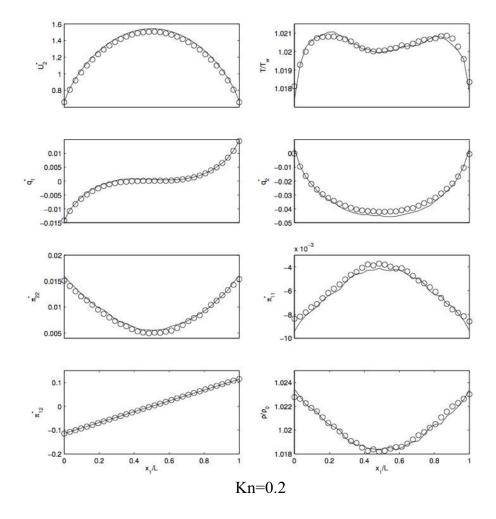
Knudsen Paradox

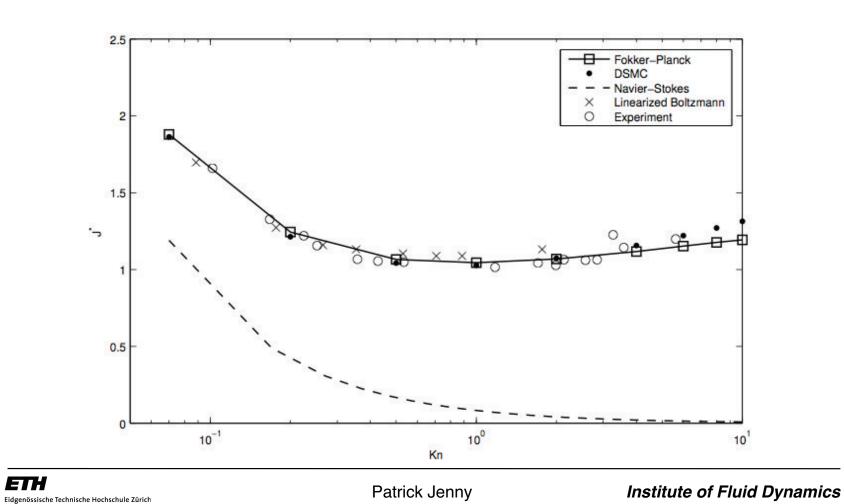




Knudsen Paradox

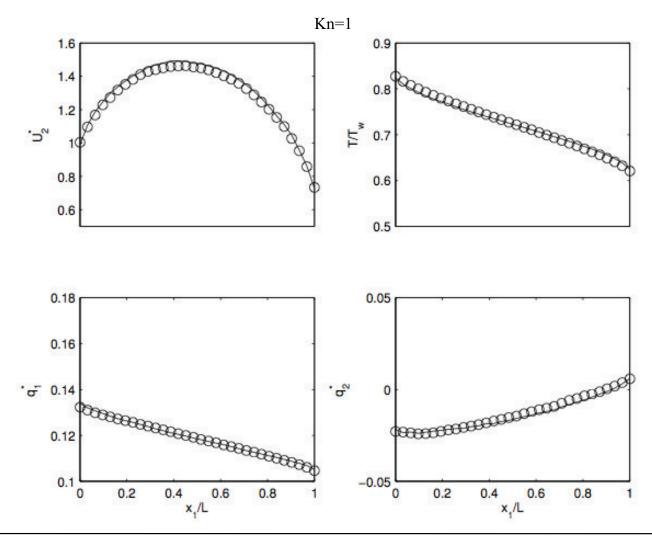






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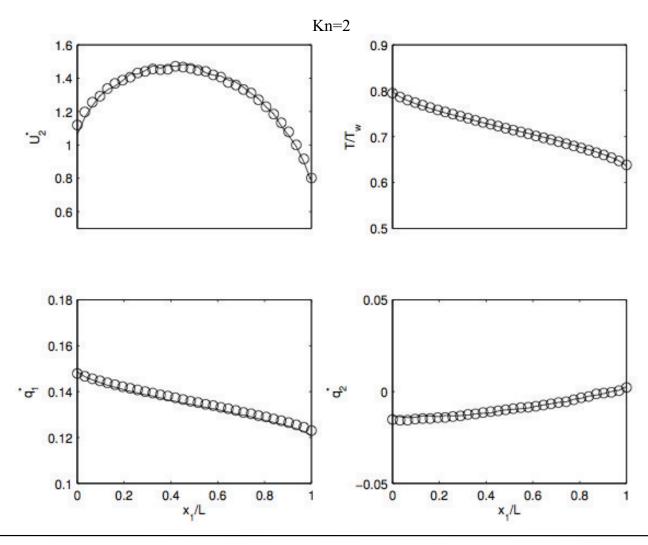


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Multiscale Modeling Framework

Continuum:

$$\begin{split} \frac{\partial \rho}{\partial t} + \frac{\partial \rho U_j}{\partial x_j} &= 0, \\ \frac{\partial \rho U_i}{\partial t} + \frac{\partial \rho U_i U_j}{\partial x_j} + \frac{\partial p_{ij}}{\partial x_j} &= \rho F_i, \\ \frac{\partial \rho e_s}{\partial t} + \frac{\partial \rho U_j e_s}{\partial x_j} + \frac{\partial q_j}{\partial x_j} + p_{jk} \frac{\partial U_j}{\partial x_k} &= 0. \end{split}$$

$$M_i^{n+1} = \dots$$

$$\Delta X_i^{n+1} = \dots$$

Conclusion

- Fokker-Planck collision operator for monatomic gas flow
- Good prediction of Knudsen paradox

- "Exact" particle integration scheme allows for large time steps
- Efficient solution algorithm
- Hybrid framework for multiscale modeling

- Prandtl number problem
- Further validation with Boltzmann and experiments